DNA supercoiling: plectonemes or curls ?

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Why study DNA mechanical properties ?

mechanical properties influence biology of the cell

- 1 meter of DNA in a 10 micron wide nucleus
- ejection from viral capside
- transcription (RNApolymerase is torque dependent)
- protein binding is strain dependent, or induces strain on DNA
- chromatin compaction/decompaction (cell division)



Pulling and twisting DNA



Pulling and twisting DNA





Pulling and twisting DNA



Data from G. Charvin (LPS-ENS)

Numerical simulations : twisted rod with self-contact



Numerical simulations : twisted rod with self-contact



(based on Swigon+Coleman model for contact in Kirchhoff rods)

S. Neukirch, "Extracting DNA ...", Phys. Rev. Lett. 93 (2004)

Limitations of the twisted rod model

1. Electrostatics repulsion : supercoiling radius R is not 1 nm

2. Tails are not straight : «disorded walk» (Worm Like Chain) Analytical model with electrostatics repulsion



Analytical model with electrostatics repulsion



Analytical model with electrostatics repulsion : results



J. Marko, "Torque and dynamics of linking number ...", Phys. Rev. E. (2007)

Statistical mechanics model







Comparing free-energies of straight and supercoiled DNA





total contour length $L = nbp \cdot 0.34 nm$



 $L = \text{nbp} \cdot 0.34 \text{ nm} = L_s + n\gamma + m(\Gamma + \ell)$

$$Free energy$$

$$L = L_s + n\gamma + m (\ell + \Gamma)$$

$$F = F_s + n F_{\gamma} + m (F_{\Gamma} + F_{\ell}) + F_f - T S$$

$$F_s = E_{twist} + E_{bend} + E_f = \frac{1}{2}C_s\tau_s^2L_s - g(f)L_s$$

$$F_{\gamma} = E_{twist} + E_{bend} = \frac{1}{2}C\tau_p^2\gamma + 4\sqrt{Af}$$

$$F_{\ell} = E_{twist} + E_{bend} + E_{electro} = \frac{1}{2}C\tau_p^2\ell + \frac{1}{2}A\frac{\sin^4\alpha}{r^2}\ell + U\ell$$

$$F_{\Gamma} = E_{twist} + E_{bend} + E_{electro} = \frac{1}{2}C\tau_p^2\Gamma + q_b\sqrt{Af} + U\Gamma$$

$$F_f = 4n\sqrt{Af} + q_Dm\sqrt{Af}$$

$$Free energy$$

$$L = L_s + n\gamma + m (\ell + \Gamma)$$

$$F = F_s + n F_{\gamma} + m (F_{\Gamma} + F_{\ell}) + F_f - T S$$
corrections to the work of the external force entropic terms

$$\begin{split} U &= U + \frac{1}{2} \, kT \, \left(\frac{kT}{Ar^2}\right)^{1/3} & \text{confinement in a tube} \\ F_\gamma &= F_\gamma - \frac{1}{4} \text{Log} \left(\frac{4\pi^2 A (kT)^2}{d^4 f^3}\right) & \text{loop size fluctuations} \\ & \text{(d=1nm)} \end{split}$$

$$S(L,\ell,n,m) = (n+m) \operatorname{Log} \left(\frac{L-m\ell}{\gamma} - n - m \right) - \operatorname{Log} n! - \operatorname{Log} m!$$

Tonks hard core gas

Free energy

$$F = F_s + n F_\gamma + m (F_\Gamma + F_\ell) + F_f - T S$$

study F under the two constraints:



we replace au_s, L_s to obtain :

$$F_{nm} = F_{nm}\left(\alpha, r, \tau_p, \ell\right)$$

Computation method

$$\begin{split} m \neq 0 & F_{nm} = F_{nm} \left(\alpha, r, \tau_p, \ell \right) \\ m = 0 & F_{n0} = F_{n0} \left(\alpha, r, \tau_p \right) \\ \text{reference} & F_{00} = -gL + \frac{1}{2}C_s \left(\frac{2\pi Lk}{L} \right)^2 L \end{split}$$

$$\Delta F_{nm}(\alpha, r, \tau_p, \ell) = F_{nm} - F_{00}$$

minimize with regard to $\ \alpha,r,\tau_p$ (saddle point approx.) plot as function of $\ \ell$



Computing mean values

At fixed Lk

Probability of seeing a configuration with n curls and m plectonemic parts: $P_{nm}(n = Lk) = \frac{\int e^{-F_{nm}(\ell)} d\ell}{\sum_{n,m} \int e^{-F_{nm}(\ell)} d\ell}$

Mean extension of the system (considering all possible configurations:

$$\langle X \rangle (n = Lk) = \frac{\sum_{n,m} \int X_{nm}(\ell) e^{-F_{nm}(\ell)} d\ell}{\sum_{n,m} \int e^{-F_{nm}(\ell)} d\ell}$$





(Phys. Rev. Let.) 2008



(Phys. Rev. Let.) 2008



Work was done with:

N. Clauvelin

- B. Audoly
- J. Marko

Funding/positions thanks to: J.M.T. Thompson G. van der Heijden J. H. Maddocks M. Ben Amar G. Maugin