

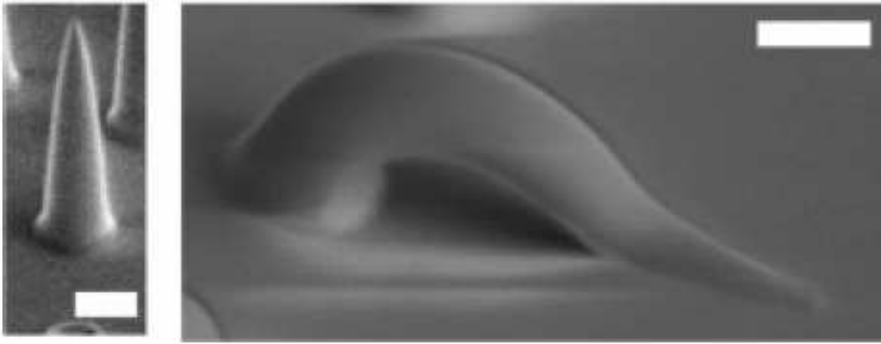
# Elasto-capillary coupling: piercing a liquid surface with an elastic rod

Sébastien Neukirch (LMM : CNRS & Univ. Paris 6)

*joint work with:* José Bico & Benoît Roman (PMMH : CNRS & ESPCI)

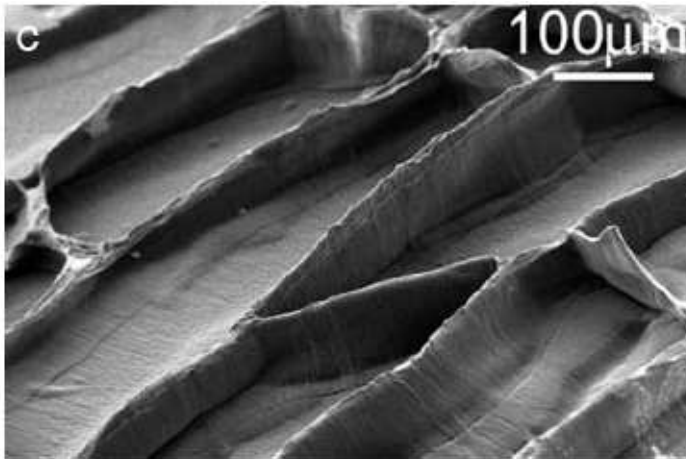


## (Some) Related works



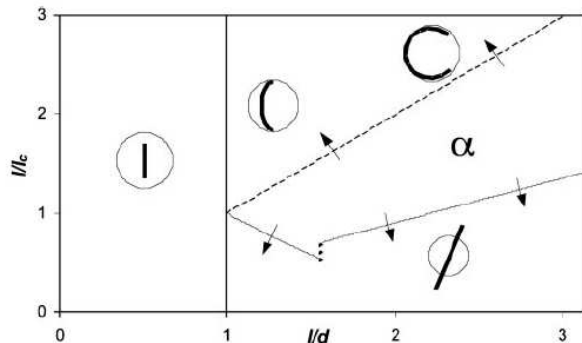
PDMS posts in water and ethanol  
(SEM images)

P. Roca-Cusachs & al., *Langmuir* (2005)



Carbon nanotubes collapse into bundles  
after liquid evaporation

N. Chakrapani & al., *Nature* (2004)



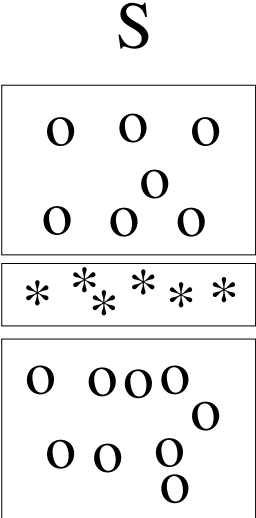
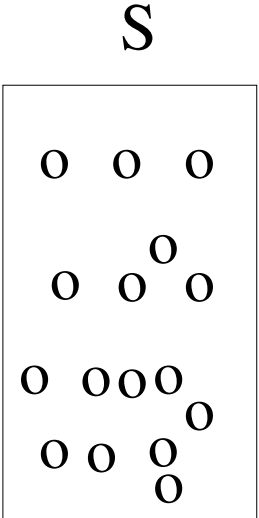
Rod in a bubble

A. Cohen & al., *PNAS* (2003)

# Capillarity

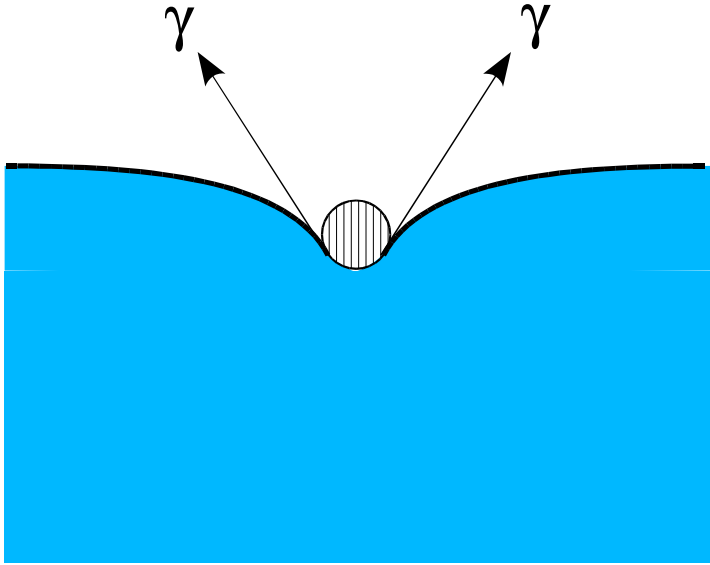
surface energy

surface tension



$$E_o - E_{o,*} = -\gamma (2S)$$

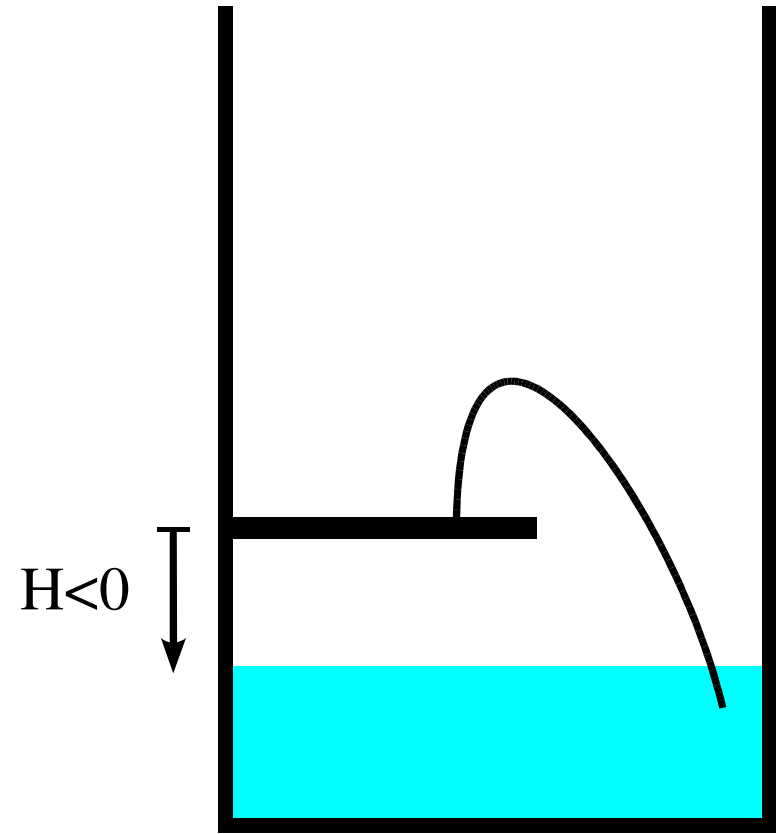
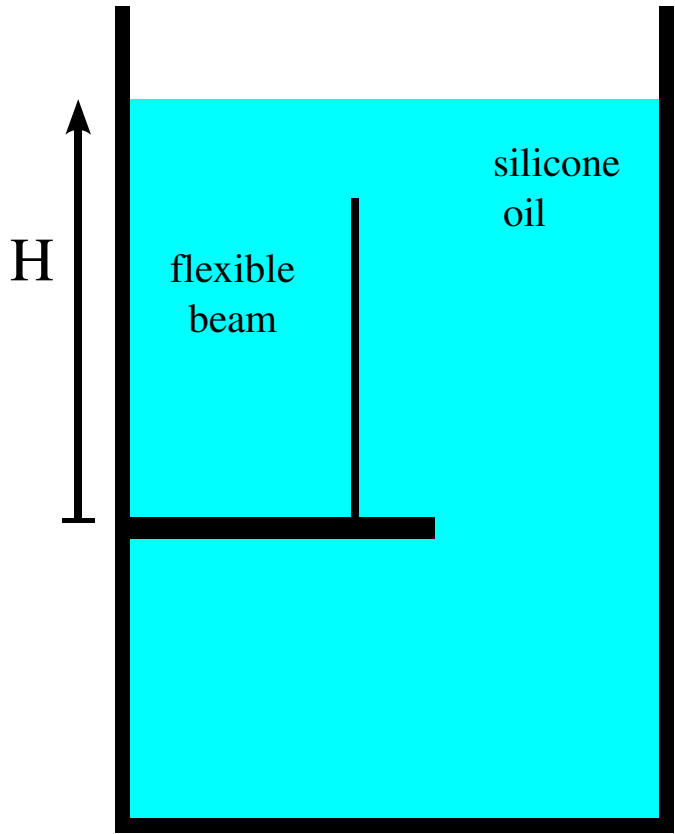
energy cost:  $\gamma$  per surface area



force  $\gamma$  per unit length

perfect wetting :  $\gamma = \gamma$  (water-air)

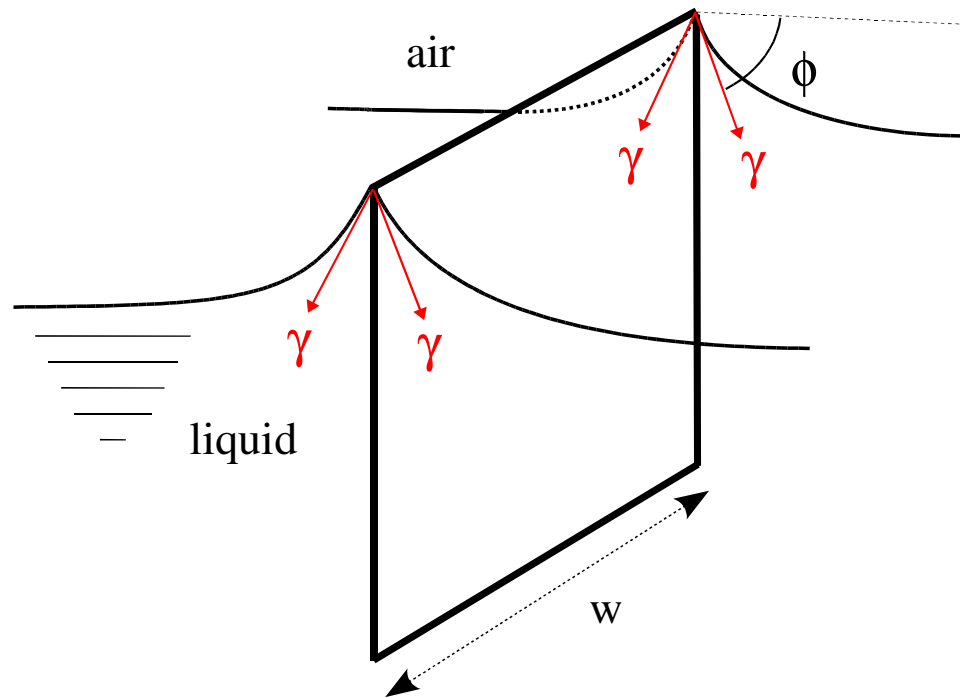
# Experimental setup



oil perfectly wets the beam

beam: polyester

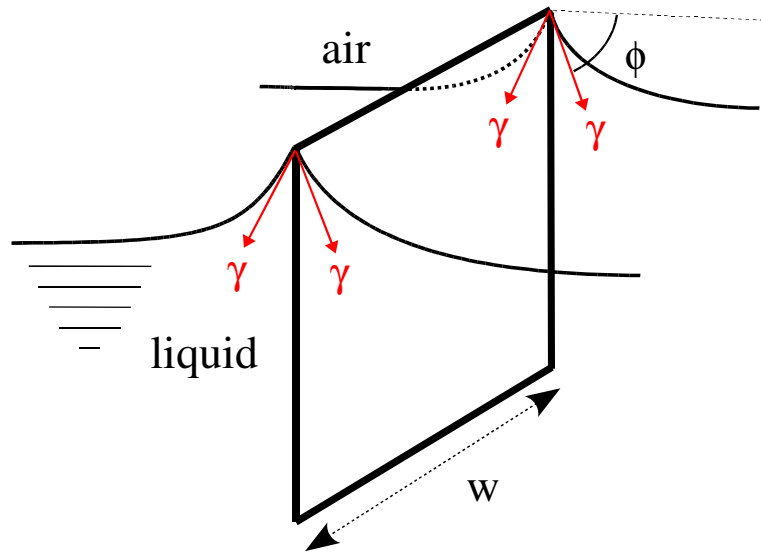
# Capillary forces on an immersed beam



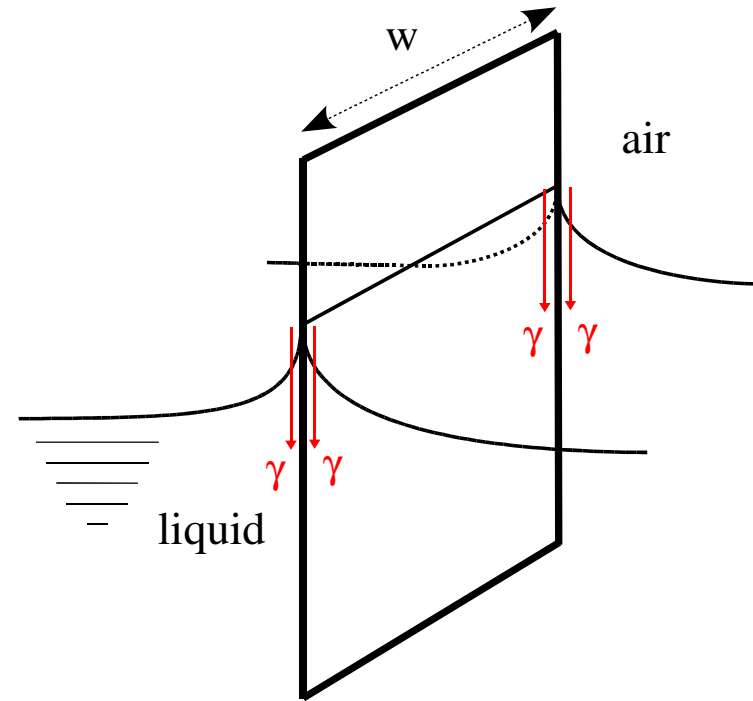
$$F_{tot} = 2 \gamma w \sin \phi$$

(thickness omitted)

# Capillary forces on an immersed beam



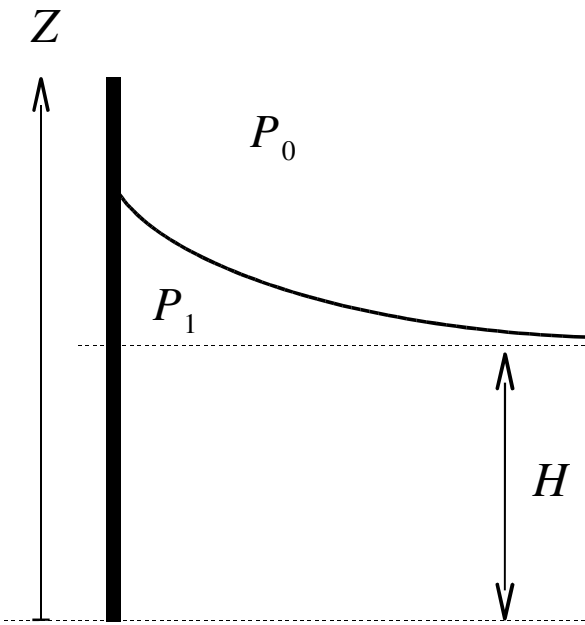
$$F_{tot} = 2 \gamma w \sin \phi$$



$$F_{tot} = 2 \gamma w$$

perfect wetting conditions

# Meniscus shape (2D)

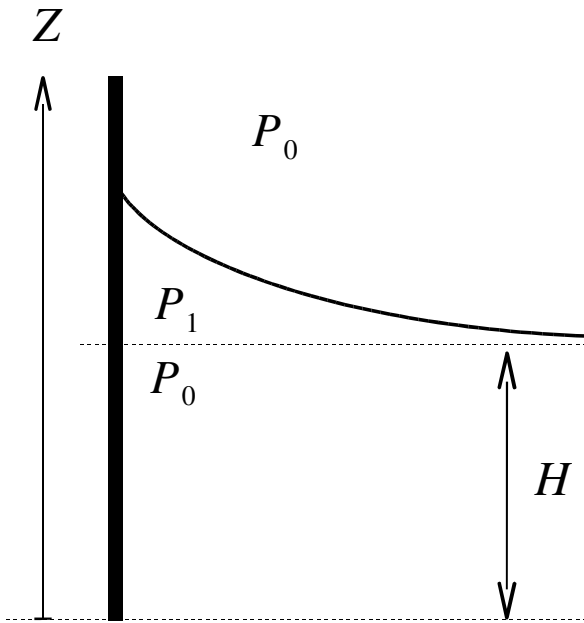


$$\Delta P = P_0 - P_1 = \gamma \kappa \quad (\text{Laplace})$$

meniscus curvature



# Meniscus shape (2D)

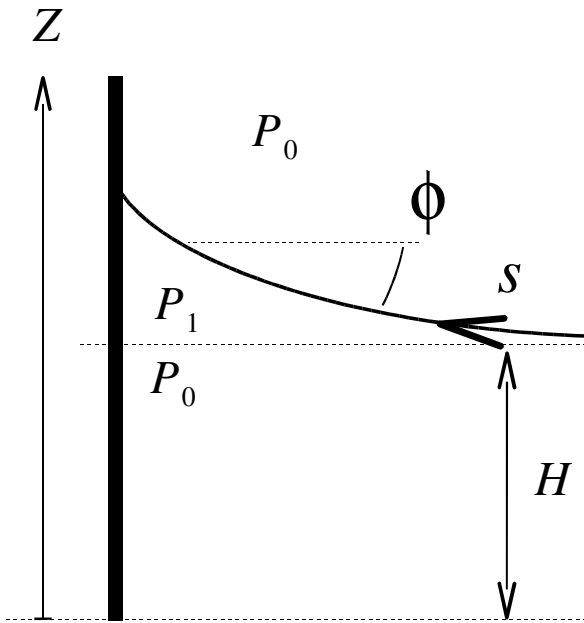


$$\Delta P = P_0 - P_1 = \gamma \kappa \quad (\text{Laplace})$$

$$\Delta P = \rho g (Z - H) \quad (\text{hydrostatics})$$



# Meniscus shape (2D)



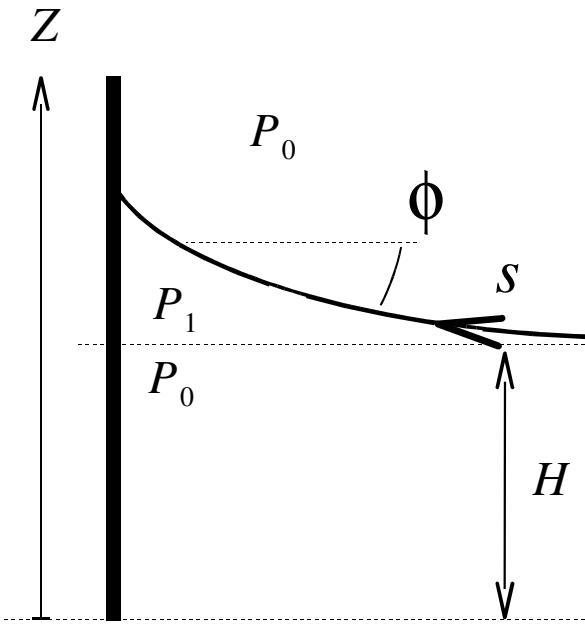
$$\Delta P = P_0 - P_1 = \gamma \kappa \quad (\text{Laplace})$$

$$\Delta P = \rho g (Z - H) \quad (\text{hydrostatics})$$

$$\frac{dZ}{ds} = \sin \phi \quad \text{meniscus tangent}$$

$$\kappa = \frac{d\phi}{ds} \quad \text{meniscus curvature}$$

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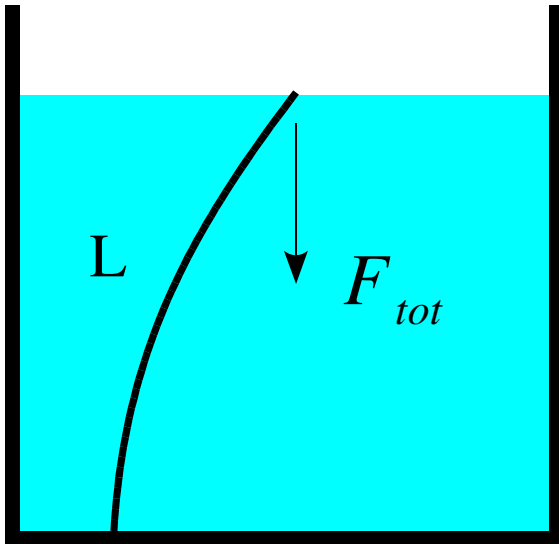
$$\kappa = \frac{d\phi}{ds} \quad \text{meniscus curvature}$$

$L_c$  : capillary length ( 1.5mm for oil-air )

$$Z(s) = H + \sqrt{2} \left( \sqrt{\frac{\gamma}{\rho g}} \right) (1 - \cos \phi(s))$$

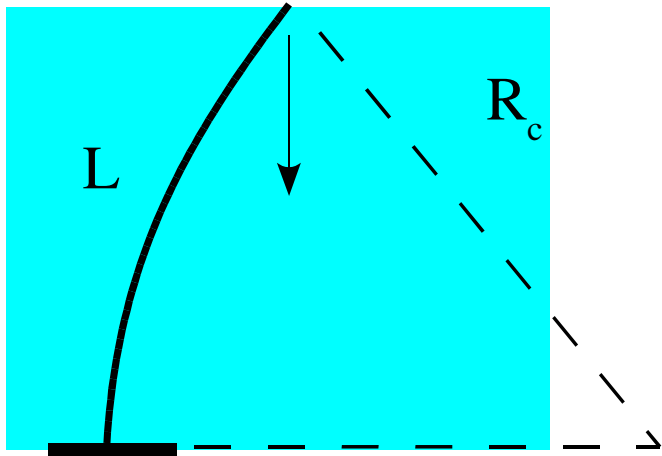
(max. meniscus height:  $\sqrt{2} L_c$ )

# Capillarity versus elasticity



$$F_{tot} \sim \gamma w$$

# Capillarity versus elasticity

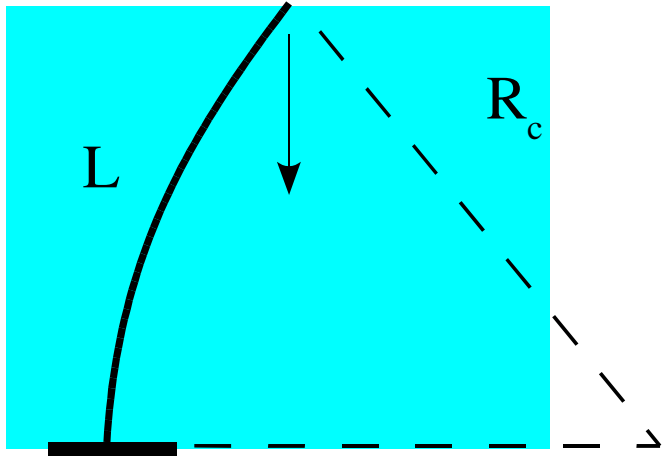


$$y_w \sim \frac{EI}{R_c} \frac{1}{L}$$

bending moment



# Capillarity versus elasticity

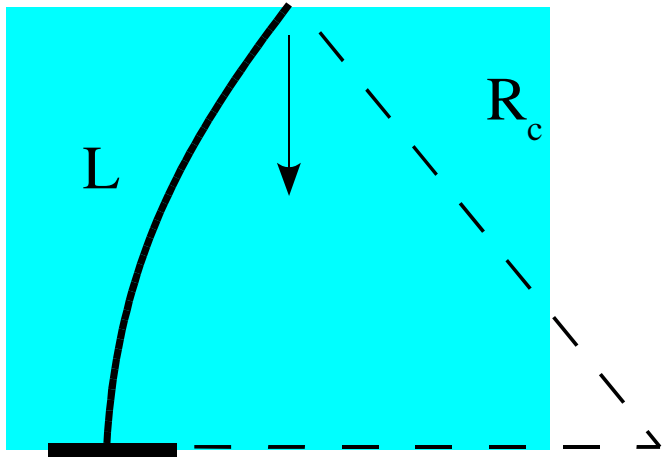


$$\gamma w \sim \frac{EI}{R_c} \frac{1}{L}$$

$$R_c \sim \sqrt{\frac{EI}{\gamma w}} \quad (\text{with } L \sim R_c)$$

↑  
Elasto-capillary length  $L_{EC}$

# Capillarity versus elasticity



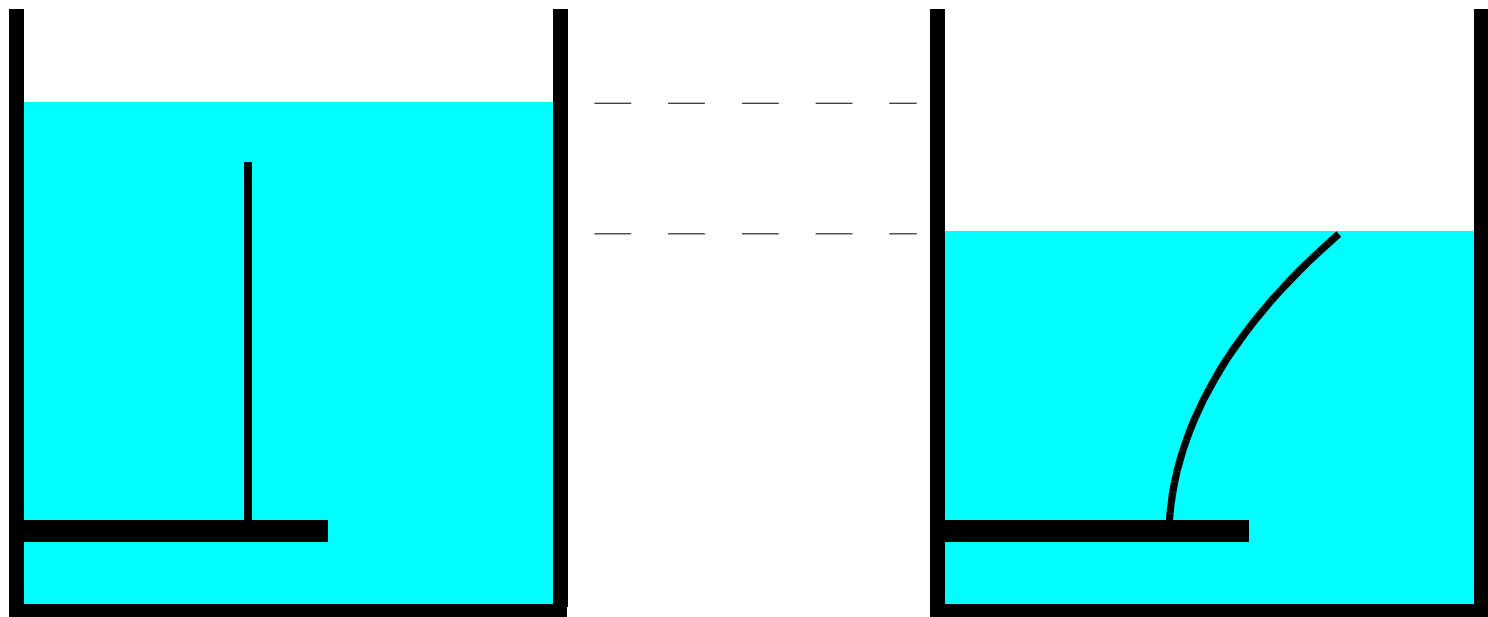
$$\gamma w \sim \frac{EI}{R_c} \frac{1}{L}$$

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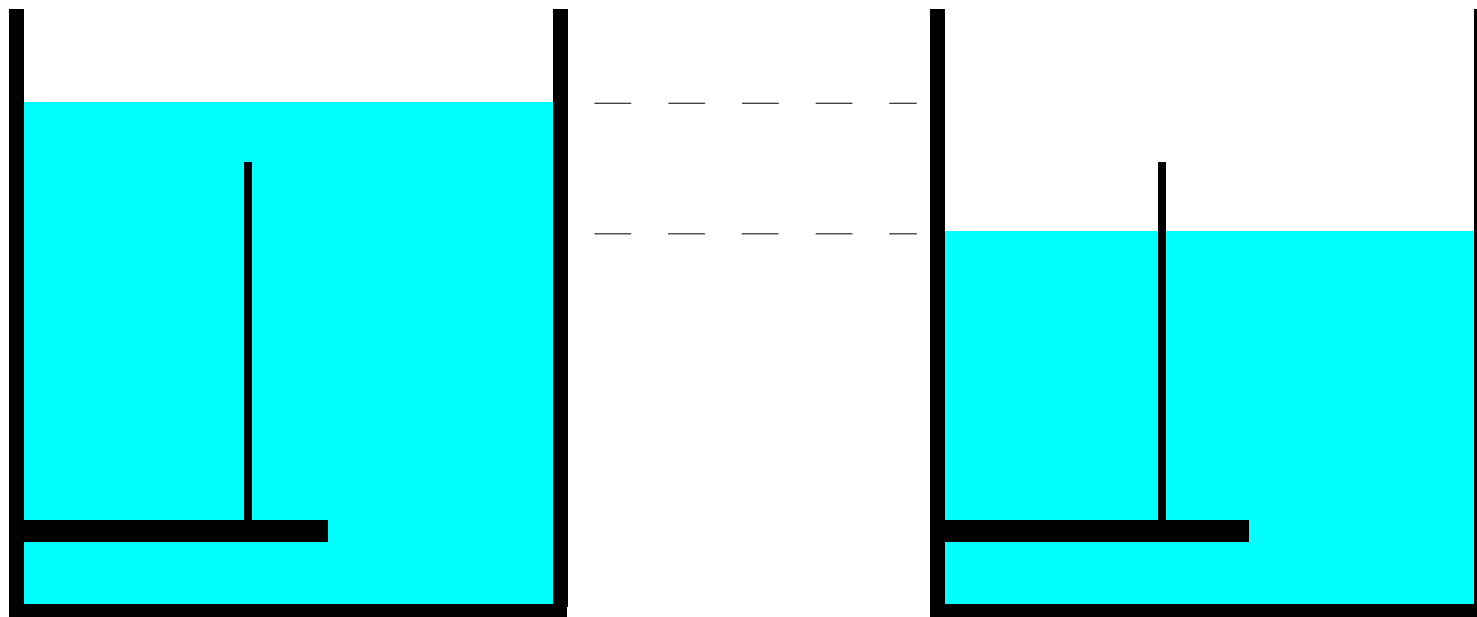
↑  
Elasto-capillary length  $L_{EC}$

if  $L \gtrsim L_{EC}$ , surface tension (largely) deflects the beam

Long enough beam



# Short beam

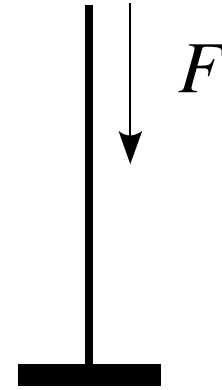




# Limiting length

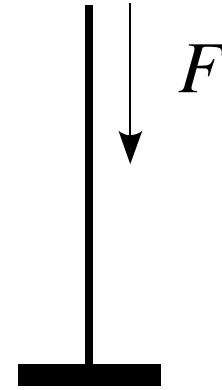
Euler buckling threshold

$$F_{euler} = \left( \frac{\pi}{2} \right)^2 \frac{EI}{L^2}$$



# Limiting length

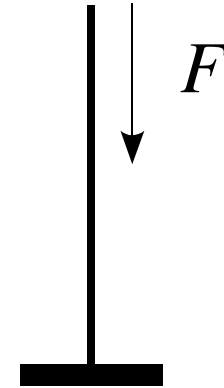
Euler buckling threshold  $F_{euler} = \left(\frac{\pi}{2}\right)^2 \frac{EI}{L^2}$



max. capillary force (on straight beam)  $F_{tot} = 2 \gamma w$

# Limiting length

Euler buckling threshold  $F_{euler} = \left(\frac{\pi}{2}\right)^2 \frac{EI}{L^2}$

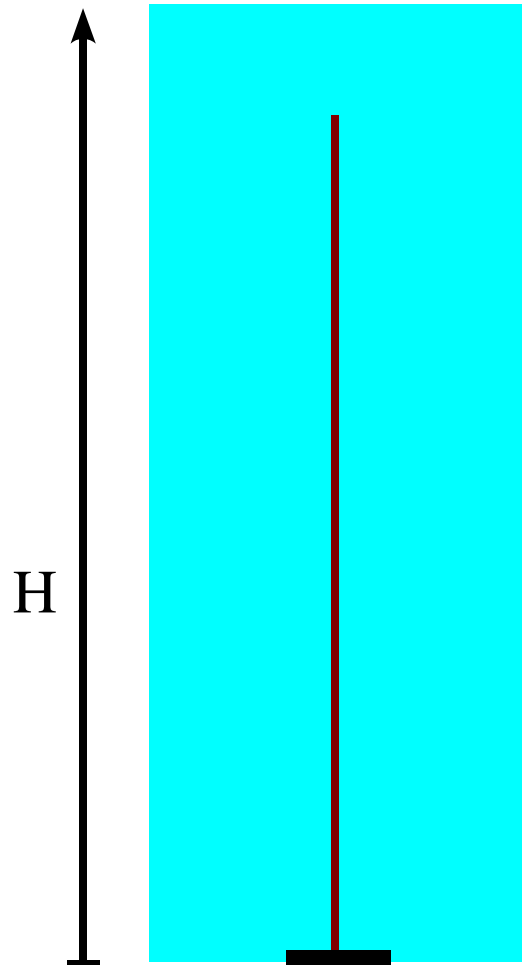
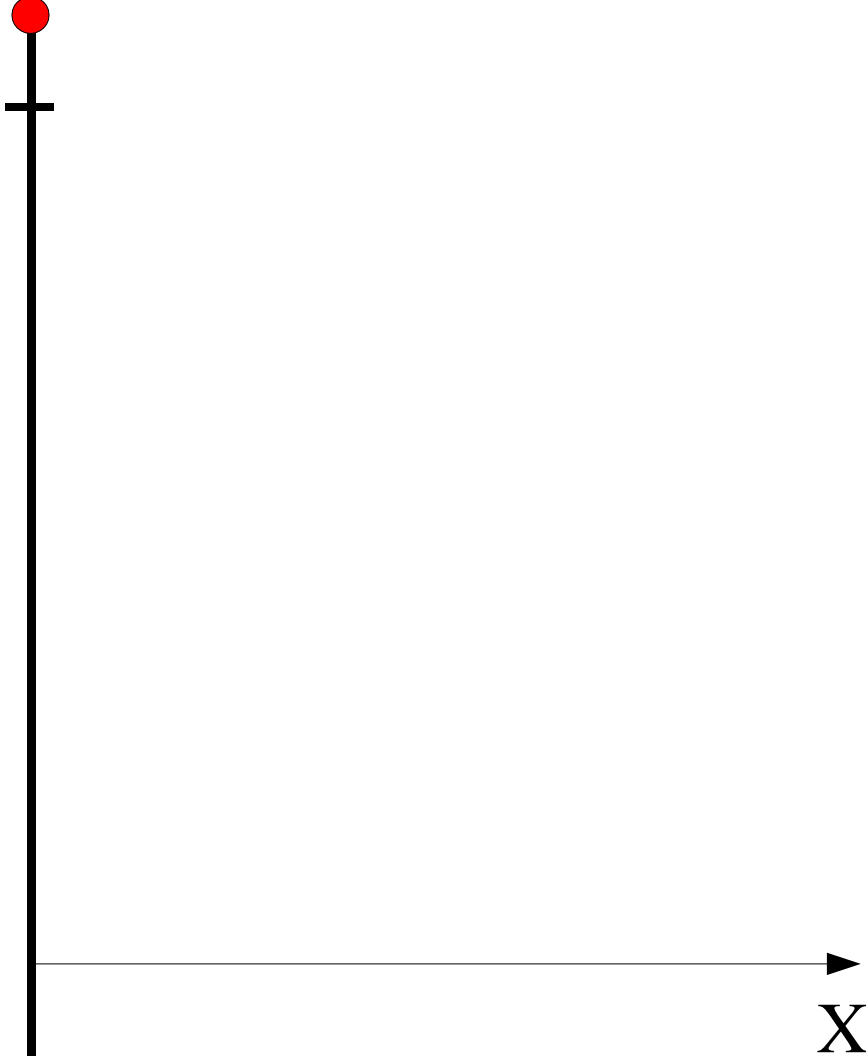
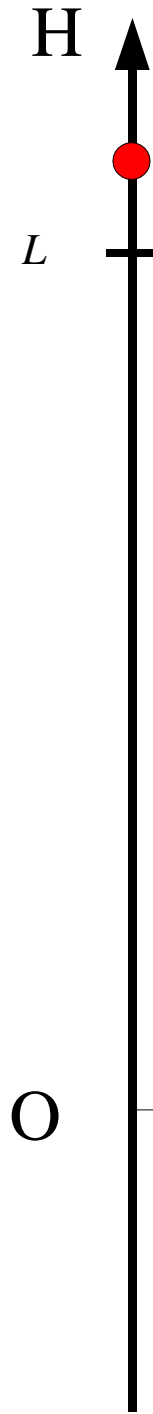


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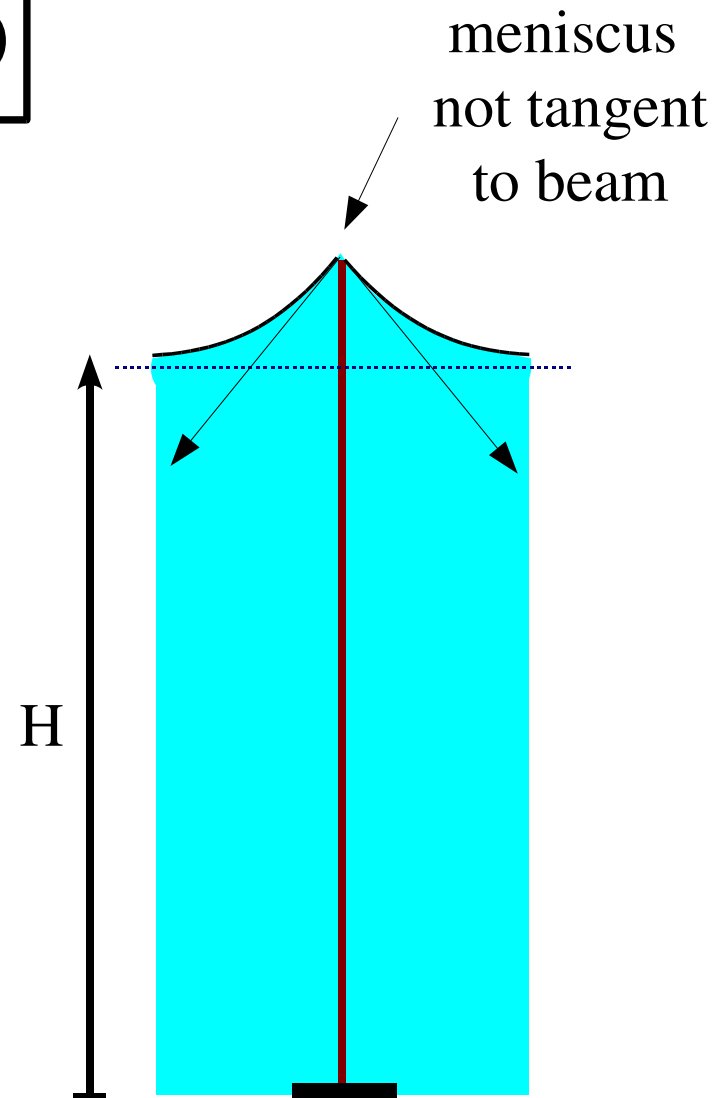
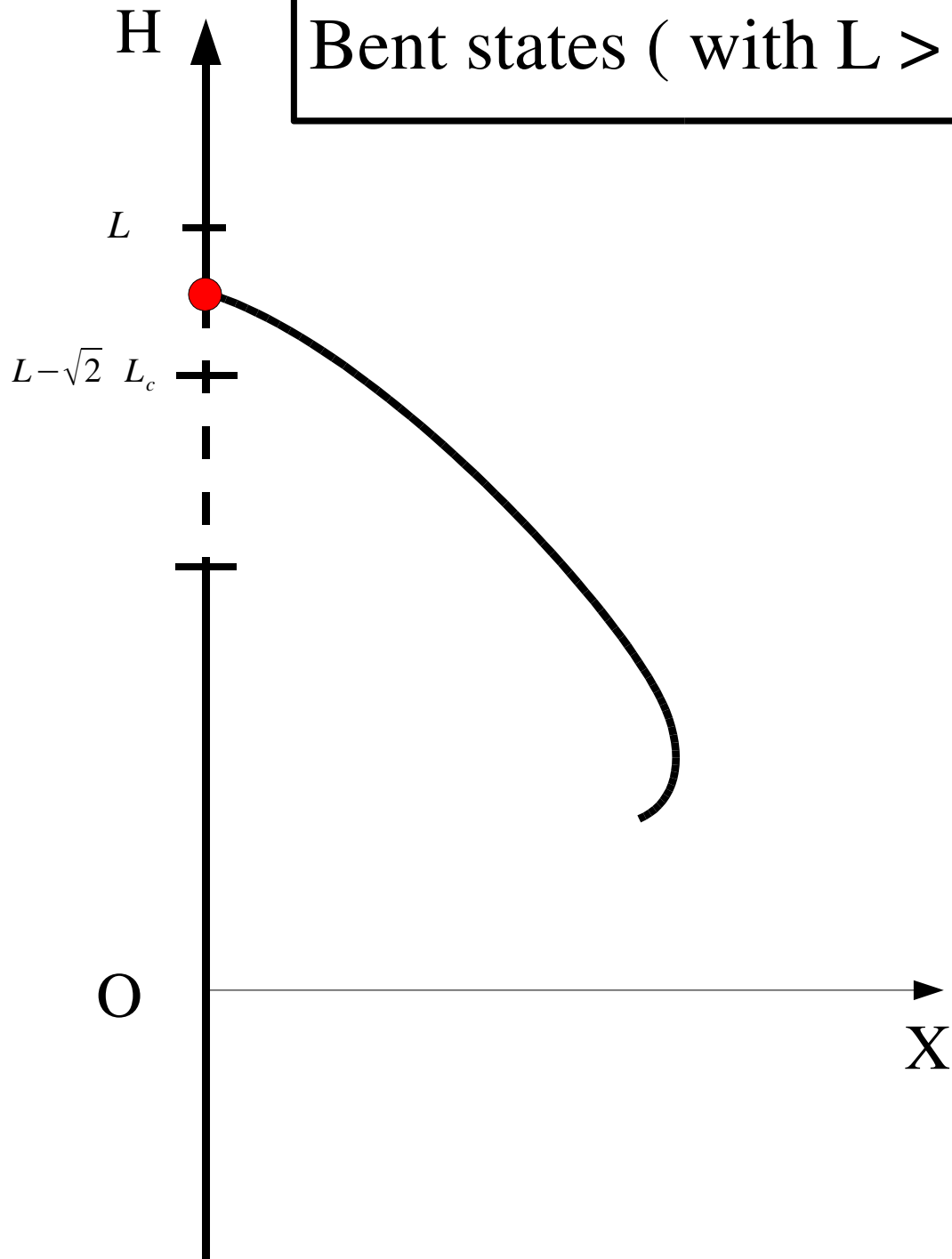
limiting length:  $L_b = \frac{\pi}{2\sqrt{2}} \sqrt{\frac{EI}{\gamma w}}$  ← Elasto-capillary length  $L_{EC}$

Bent states ( with  $L > L_b$  )

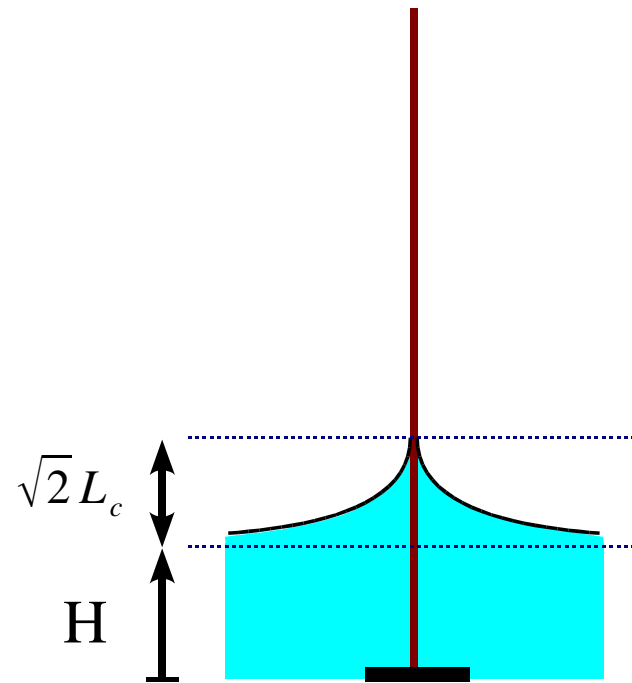
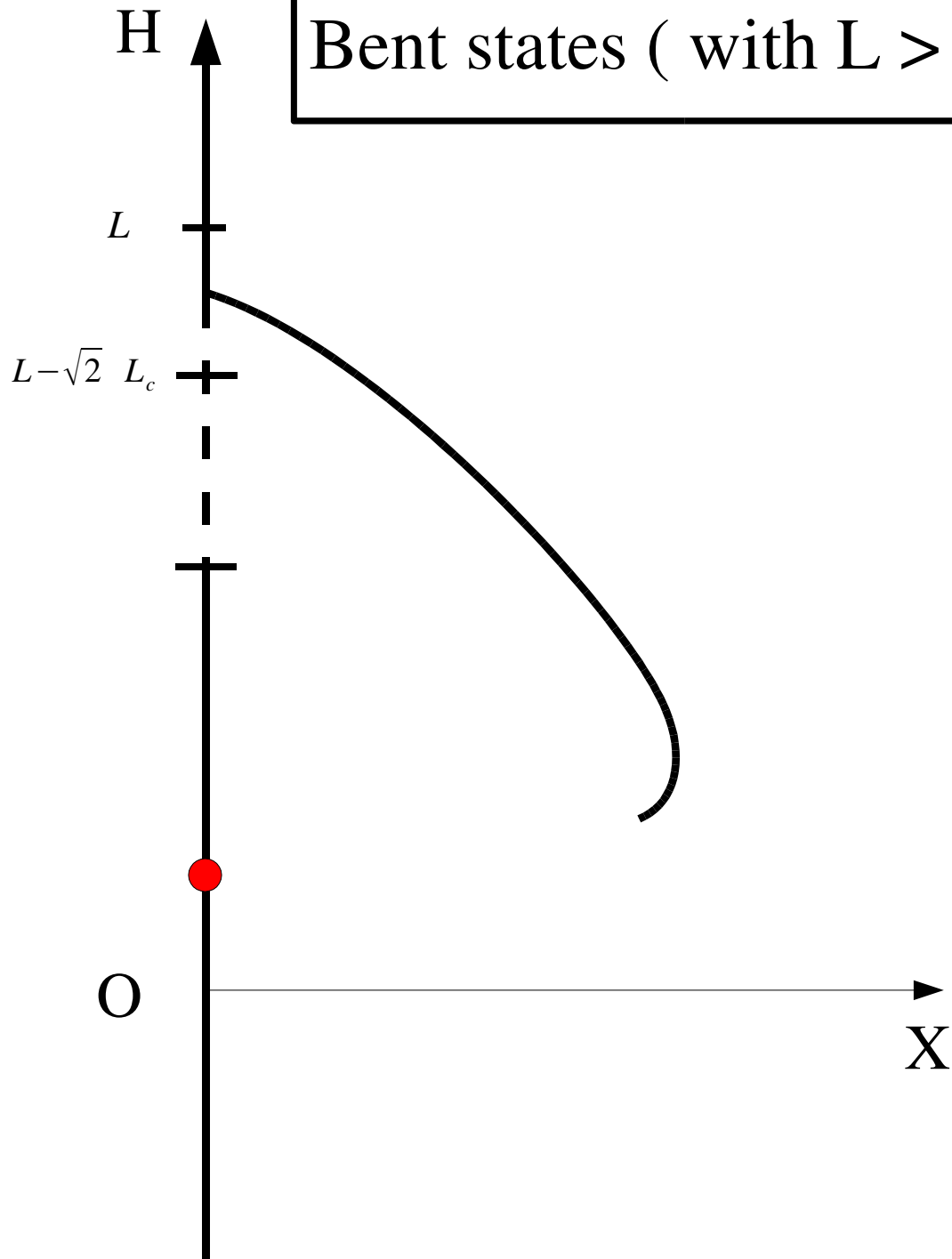


H

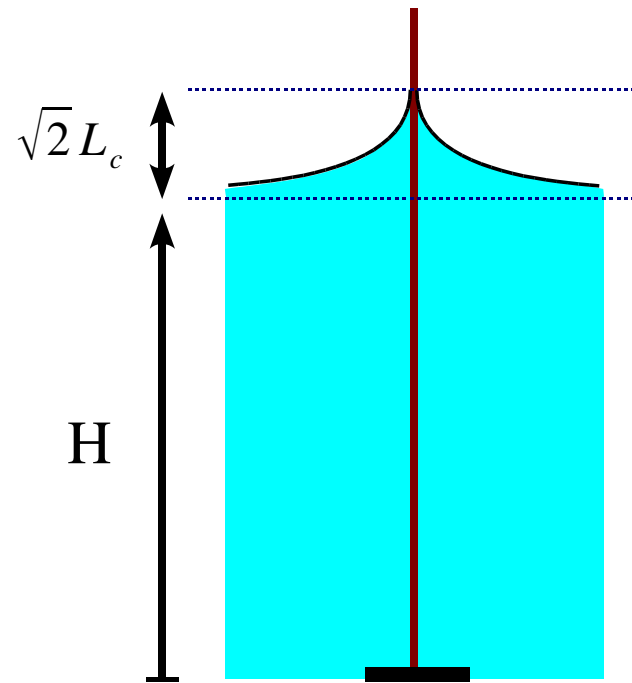
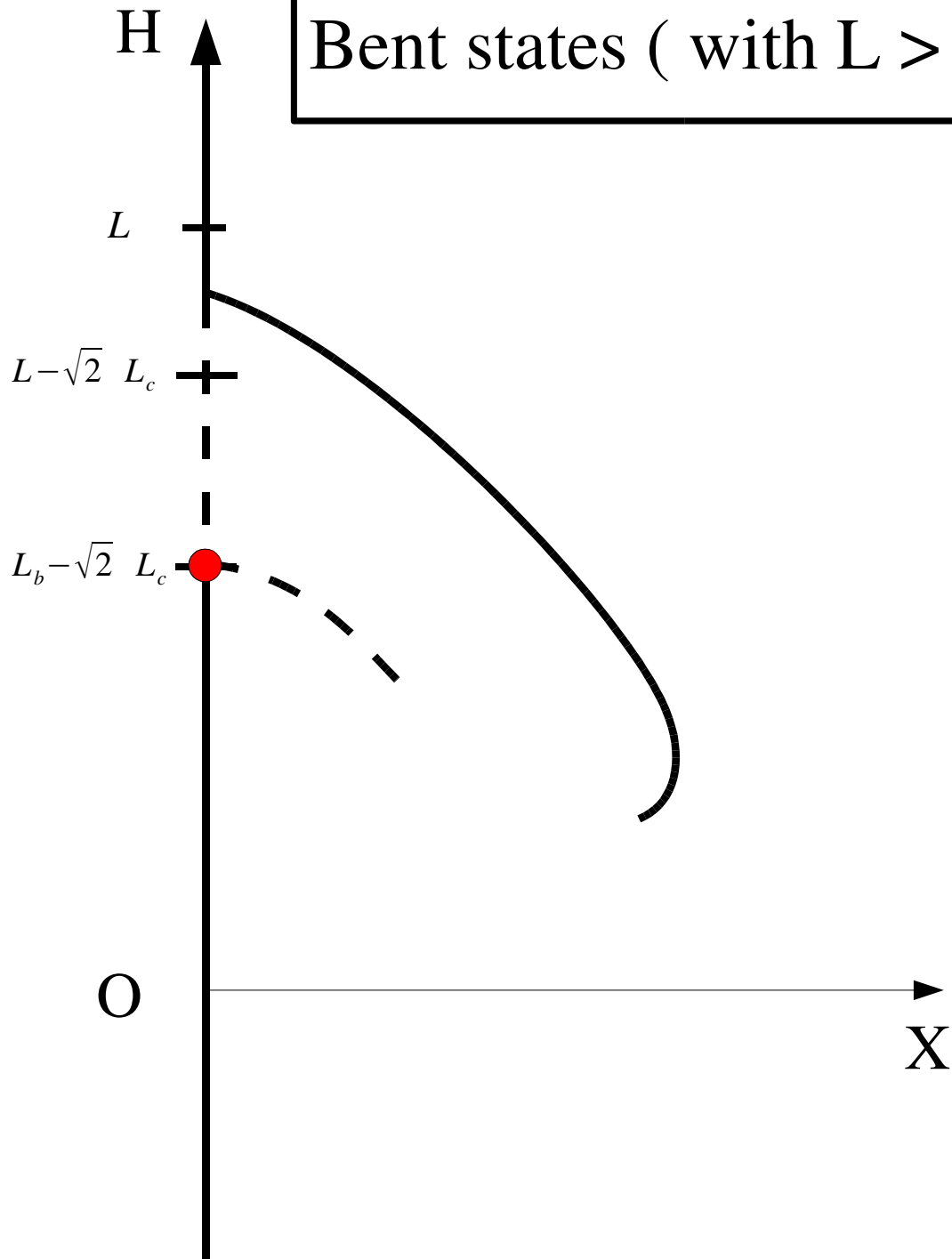
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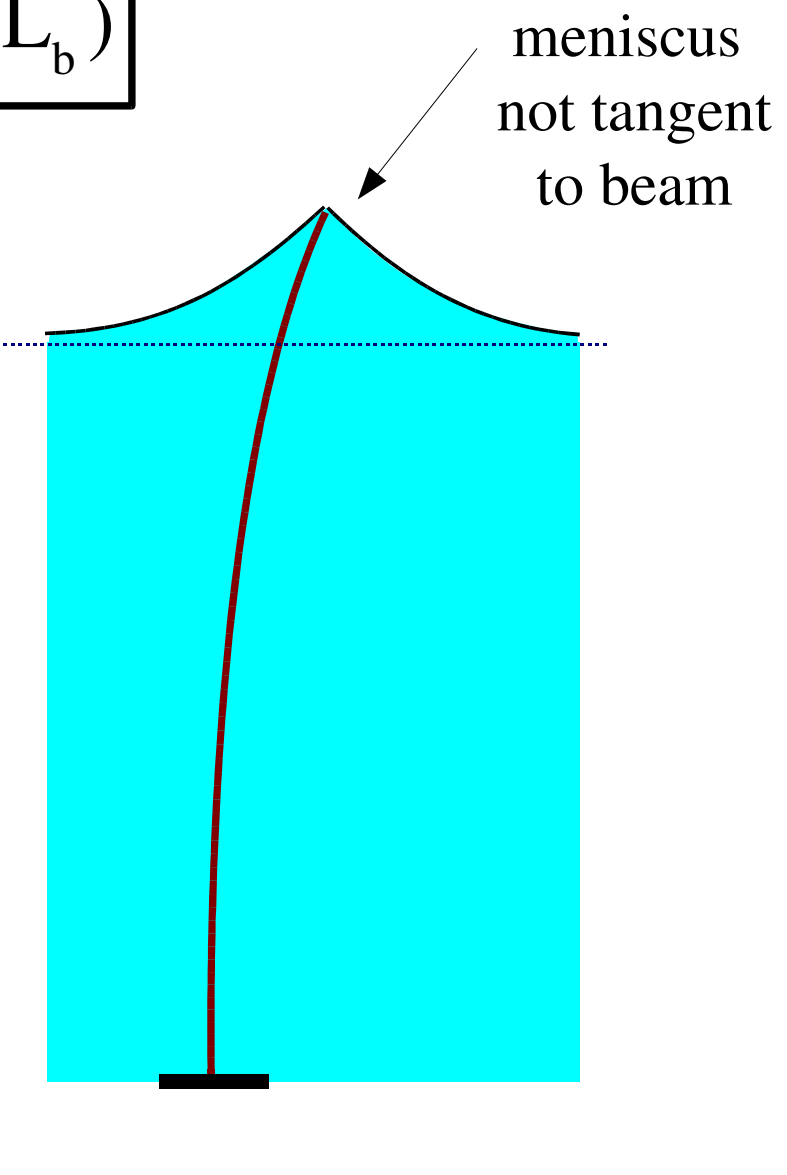
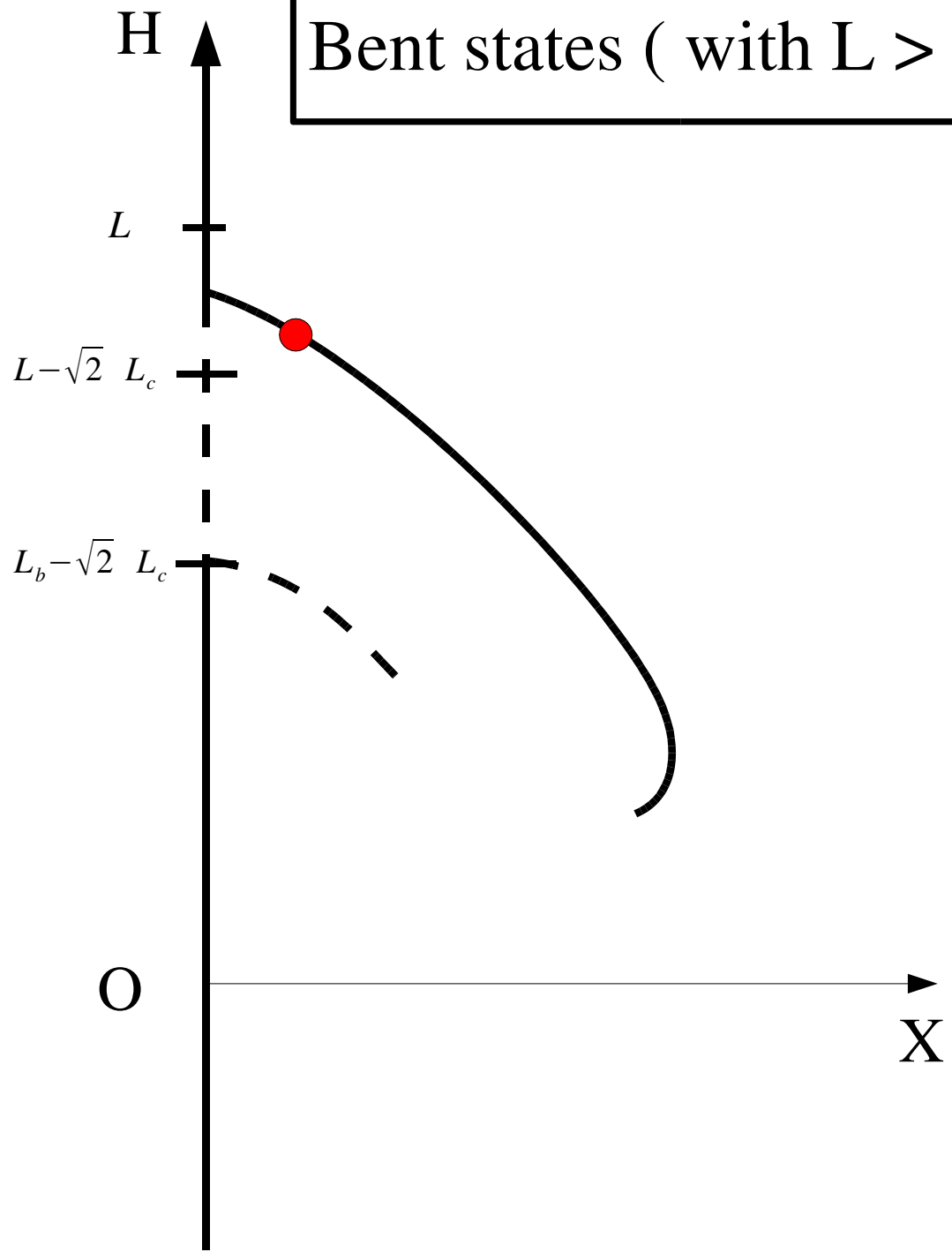
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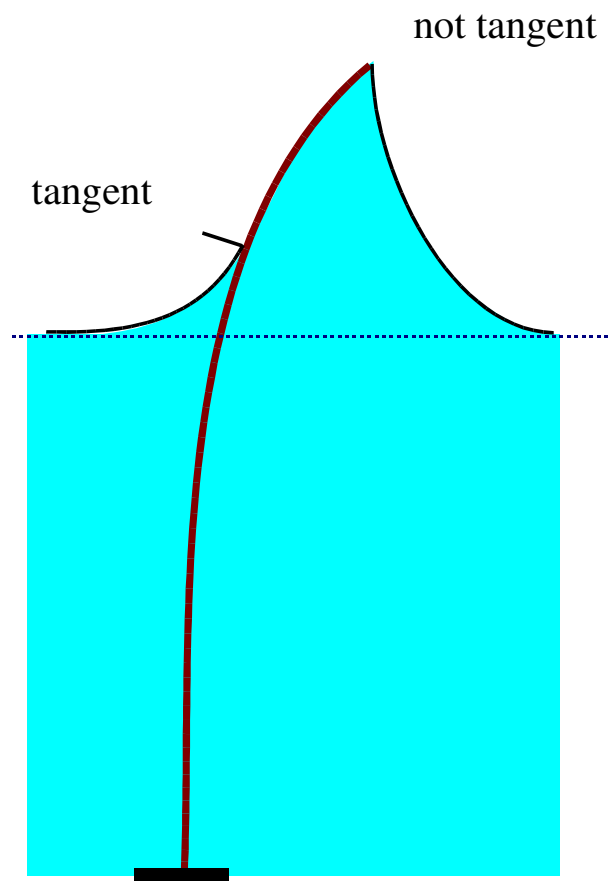
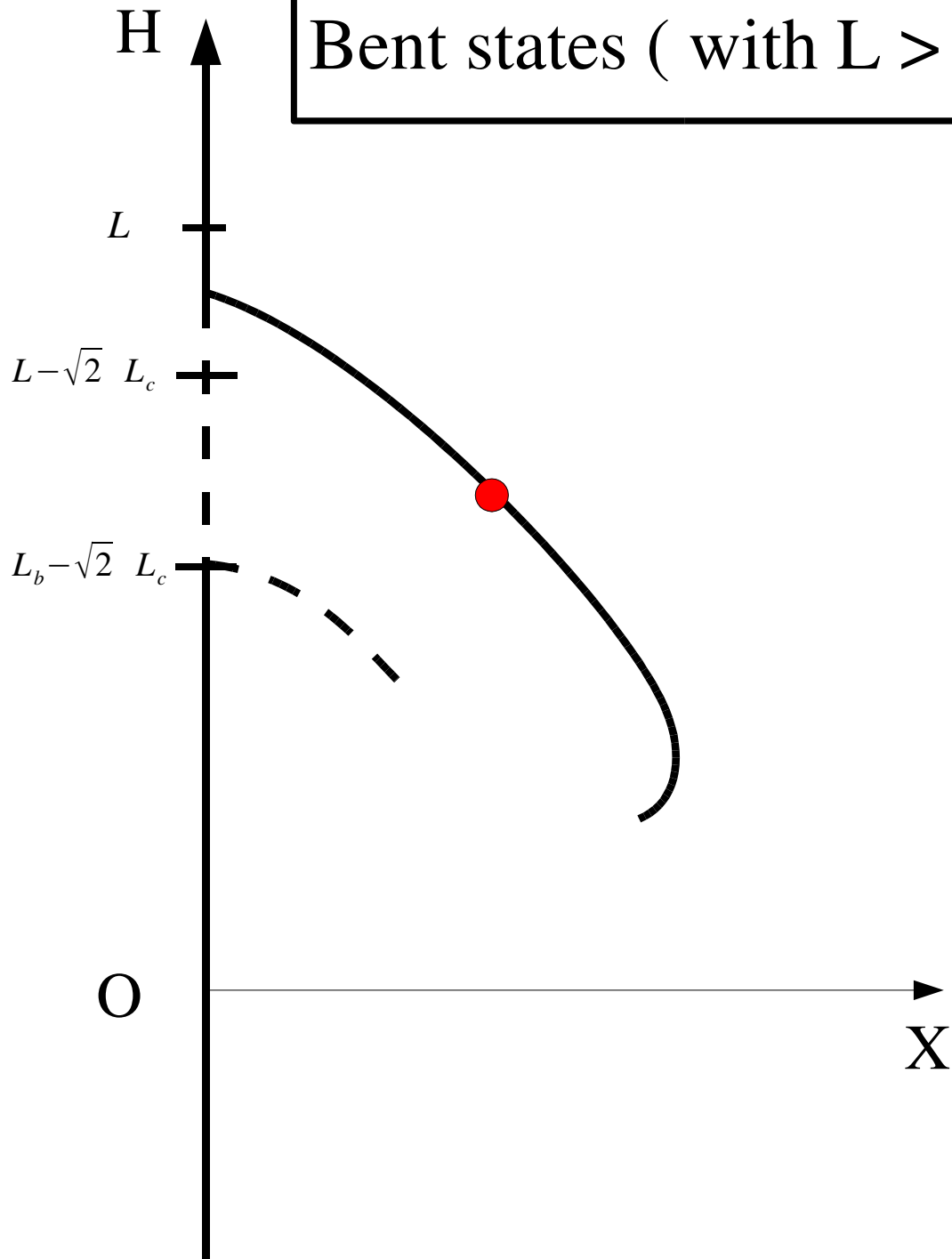


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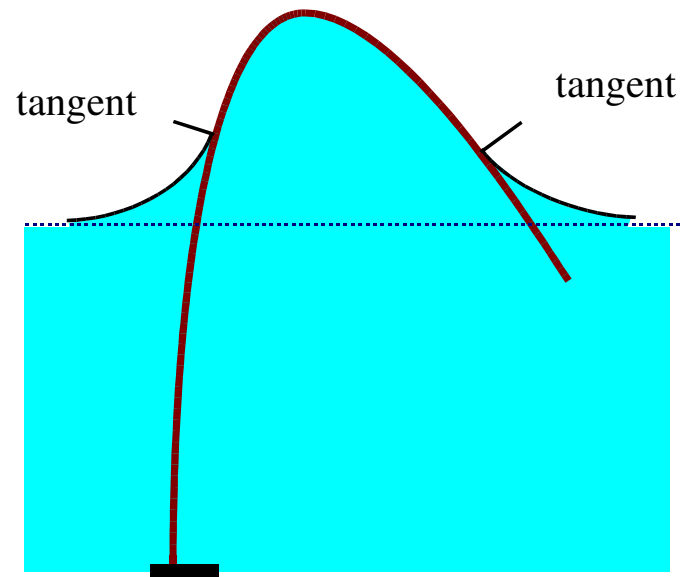
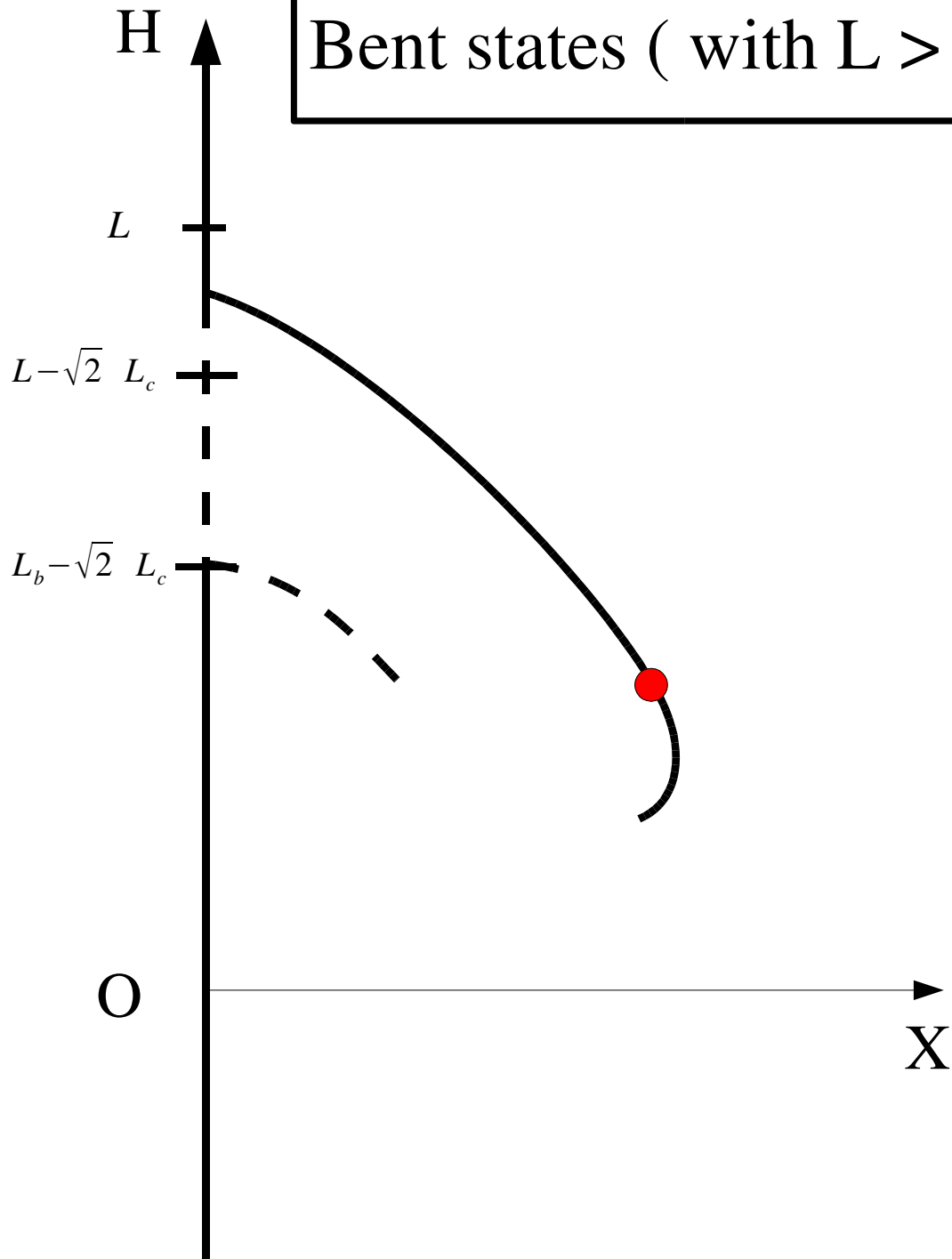




Bent states ( with  $L > L_b$  )



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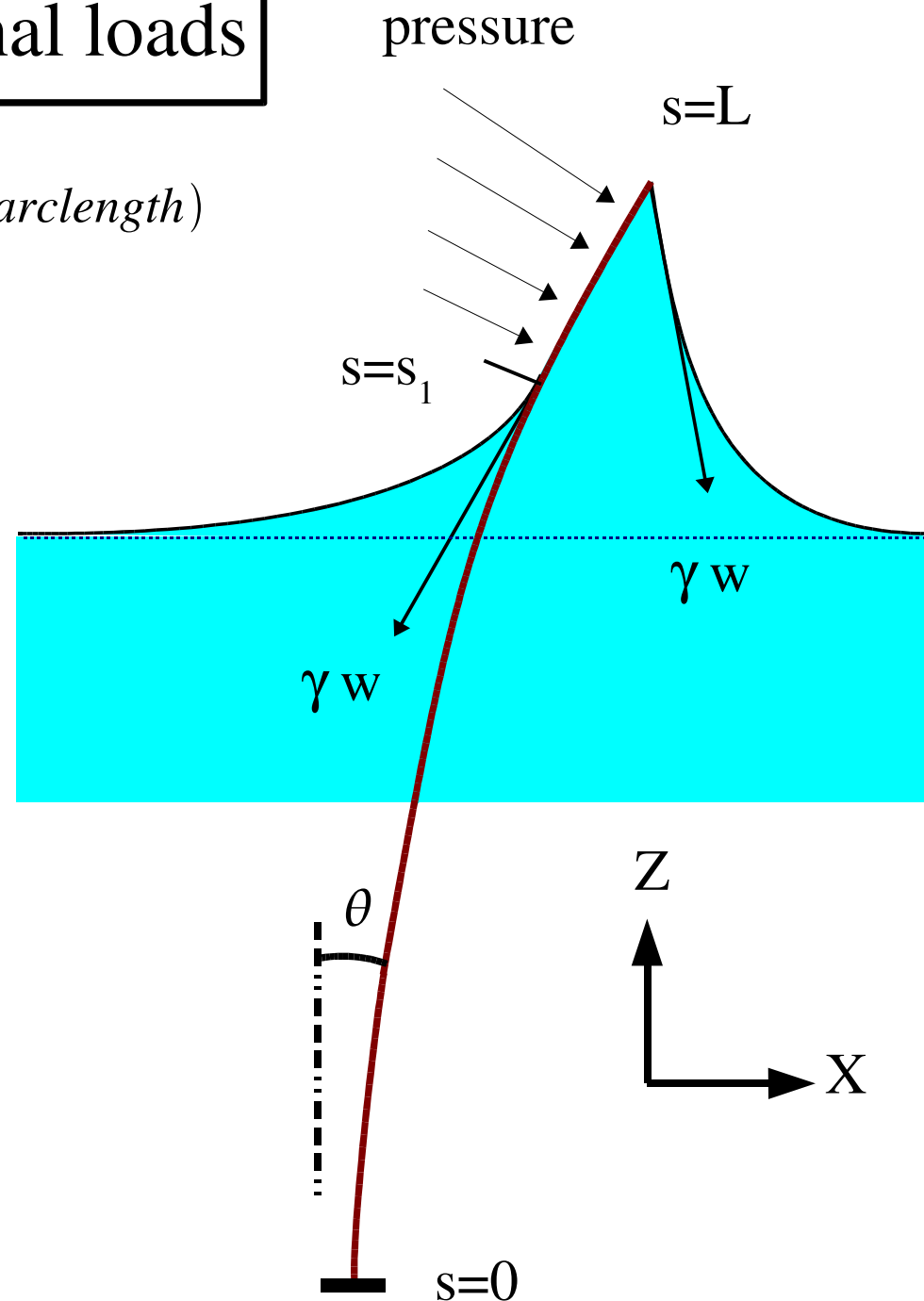
# Planar elastica with external loads

$$\left\{ \begin{array}{l} N_x' = -P_x \\ N_z' = -P_z \\ M_y' = N_z \sin \theta - N_x \cos \theta \\ X' = \sin \theta \\ Z' = \cos \theta \\ \theta' = M_y / (EI) \end{array} \right. \quad ' \equiv \frac{d}{ds} ; (s: \text{arclength})$$

$$s=0 \rightarrow s=s_1$$

$$\left\{ \begin{array}{l} P_x = 0 \\ P_z = -(\rho_b - \rho) g w e < 0 \end{array} \right.$$

buoyancy

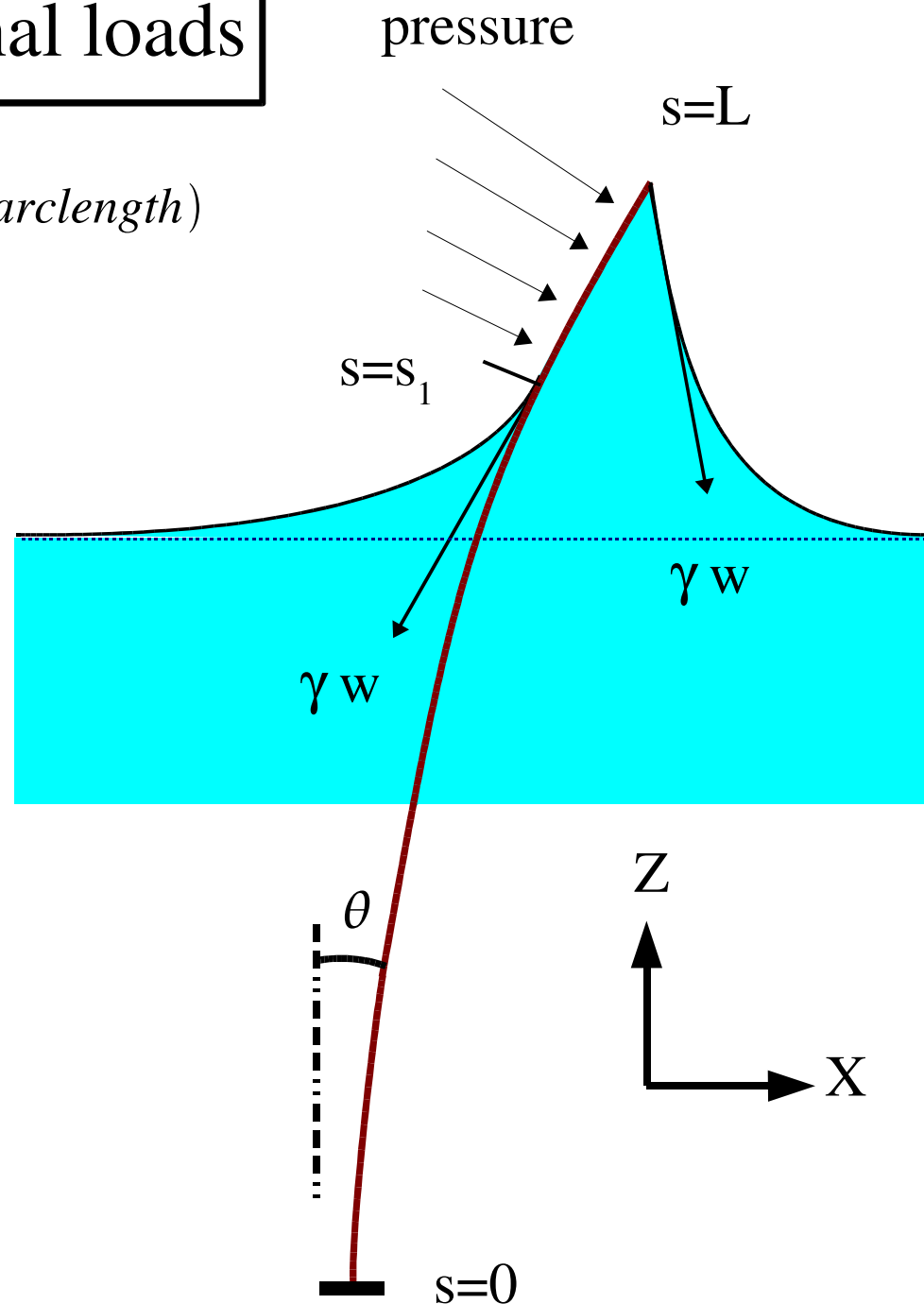


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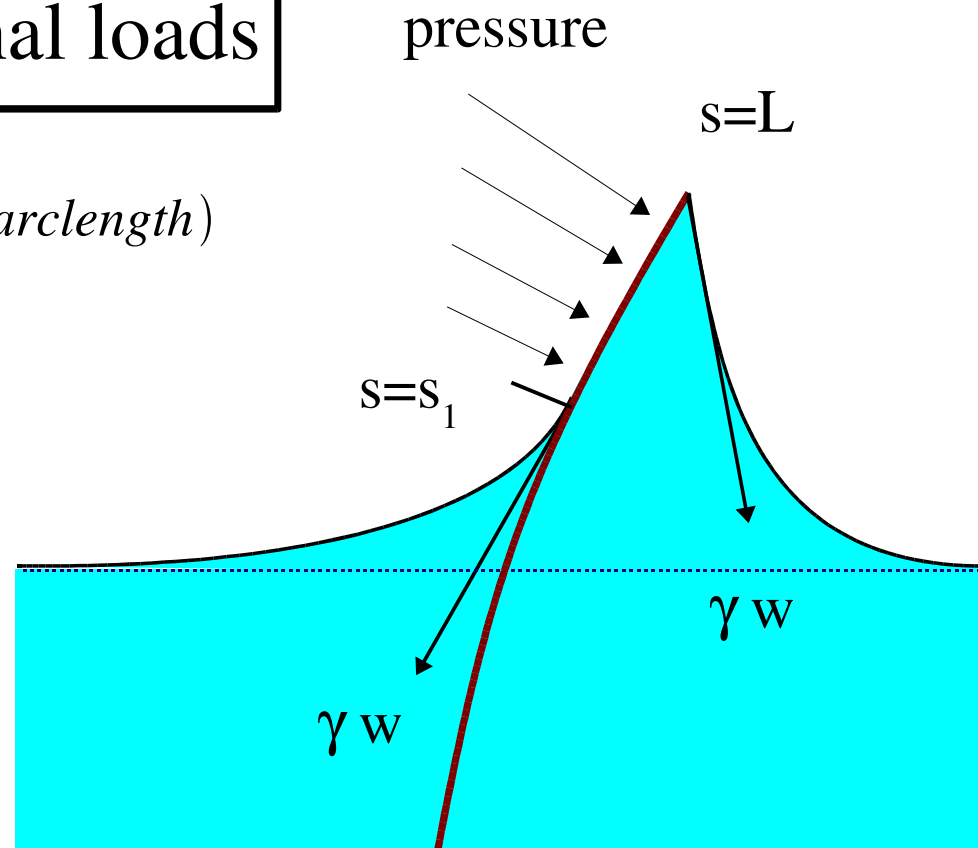
at  $s = s_1$

$$\left\{ \begin{array}{l} N_x(s_1^+) - N_x(s_1^-) = \gamma w \sin \theta(s_1) \\ N_z(s_1^+) - N_z(s_1^-) = \gamma w \cos \theta(s_1) \end{array} \right.$$



# Planar elastica with external loads

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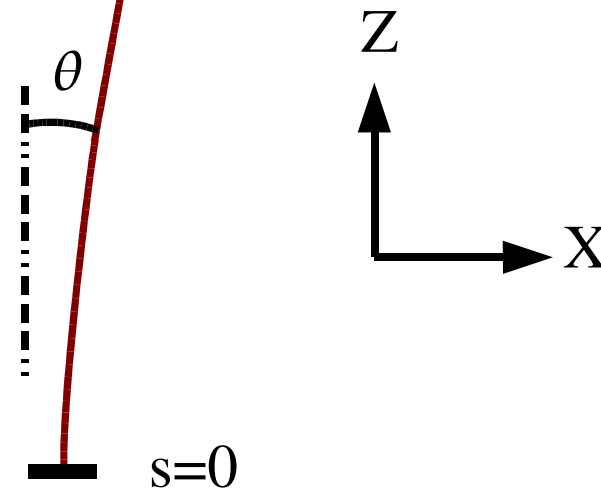


$$s = s_1 \rightarrow s = L$$

$$\left\{ \begin{array}{l} P_x = +\rho g (Z - H) w \cos \theta > 0 \\ P_z = -\rho g (Z - H) w \sin \theta - \rho_b g w e < 0 \end{array} \right.$$

↑  
pressure

↑  
weight



# Planar elastica with external loads

## Boundary conditions

$$s=0 :$$

$$X(0)=0=Z(0); \quad \theta(0)=0$$

$$s=s_1 :$$

$$Z(s_1)=H+\sqrt{2}L_c\sqrt{1-\sin\theta(s_1)}$$

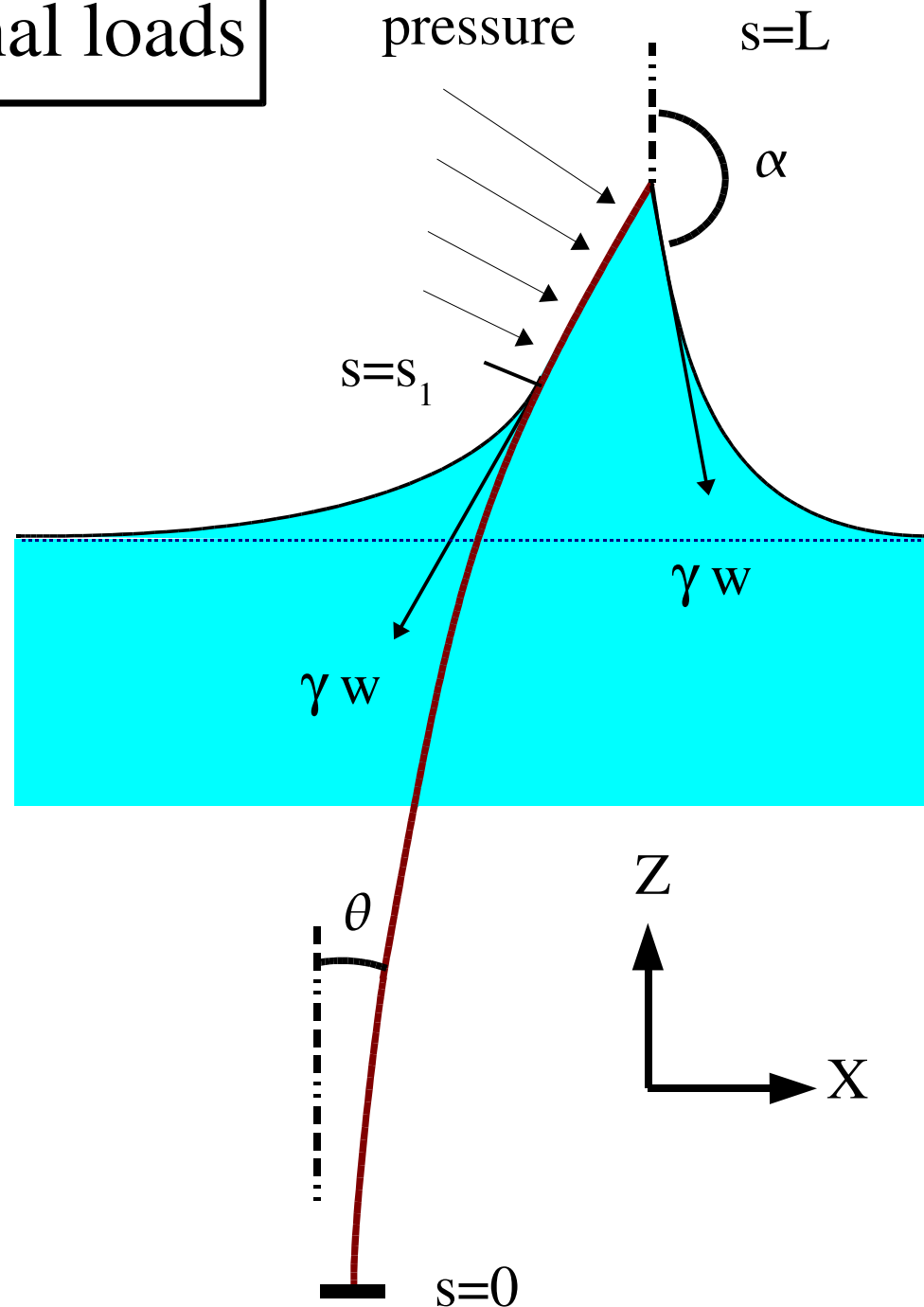
$$s=L :$$

$$M_y(L)=0$$

$$N_x(L)=\gamma w \sin \alpha$$

$$N_z(L)=\gamma w \cos \alpha$$

$$Z(L)=H+\sqrt{2}L_c\sqrt{1-\sin\alpha}$$



# Planar elastica with external loads

## Counting the shooting parameters / equations

Once the beam characteristics  
(L, L<sub>b</sub>, L<sub>c</sub>) are fixed

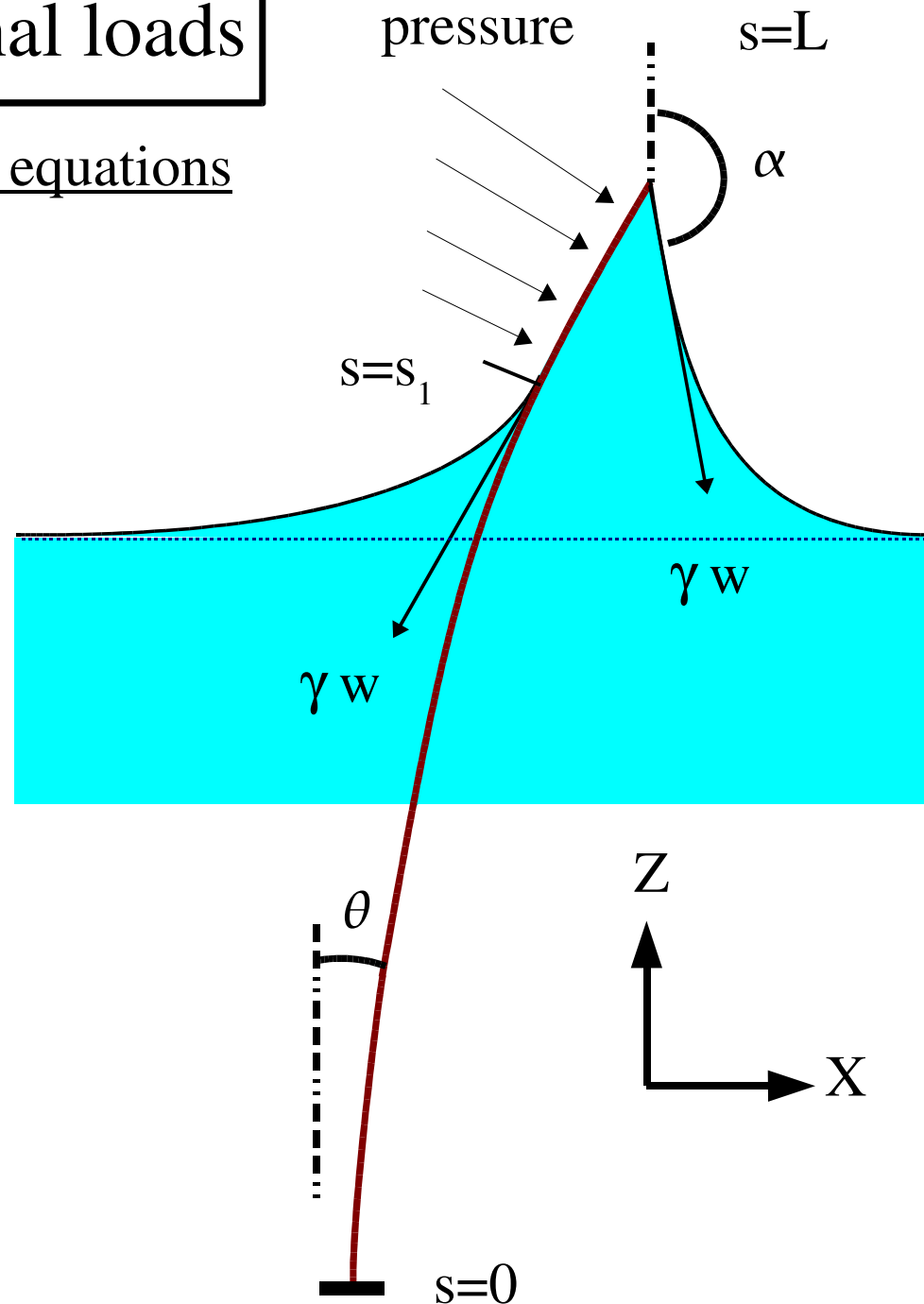
5 variables

$$M_y(0), N_x(0), N_z(0), s_1, \alpha$$

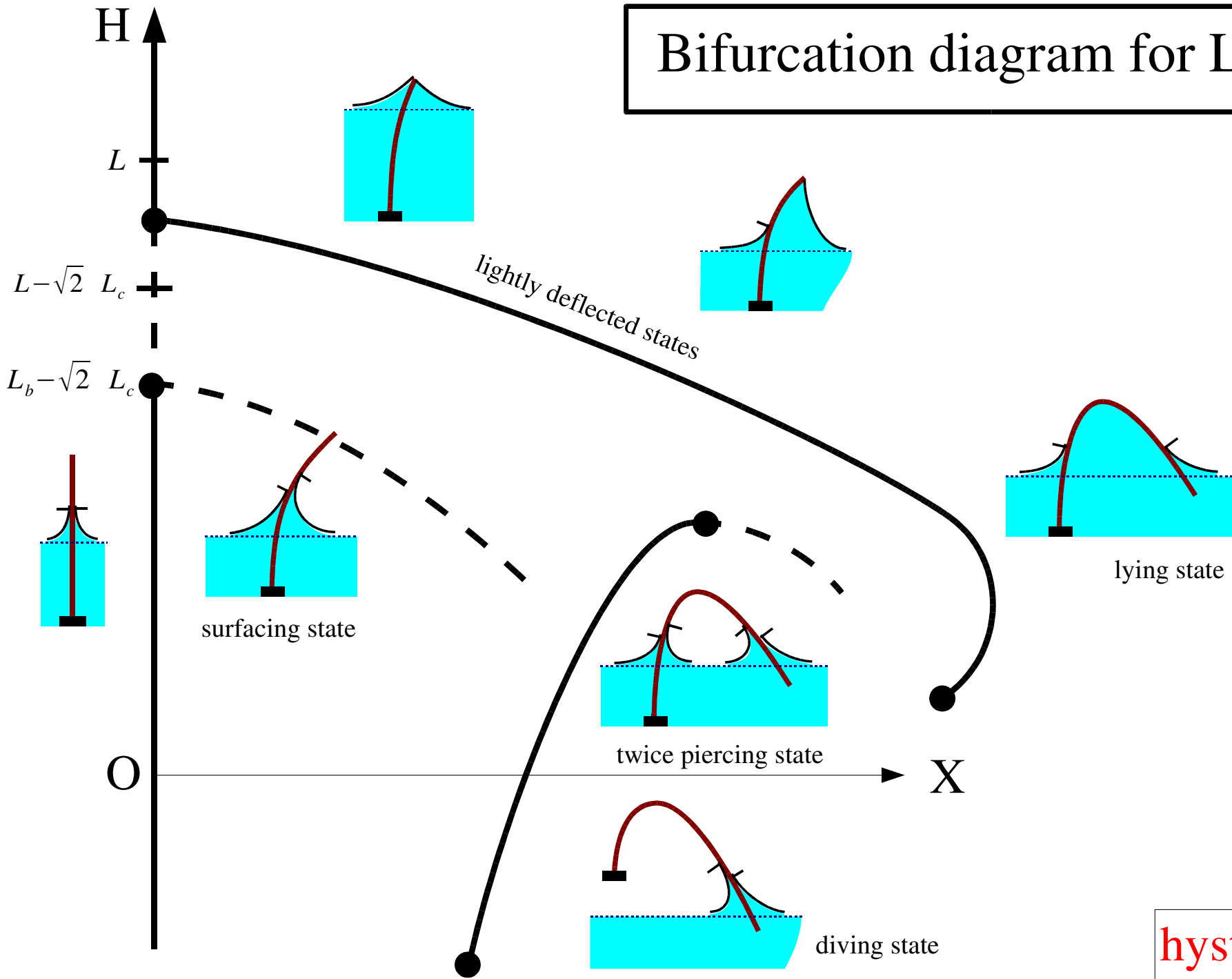
4 equations

$$M_y(L) = 0, N_x(L) = \dots, N_z(L) = \dots,$$
$$Z(s_1) - \sqrt{2} L_c \sqrt{1 - \sin \theta(s_1)} =$$
$$Z(L) - \sqrt{2} L_c \sqrt{1 - \sin \alpha}$$

**=> 1D solution manifold**



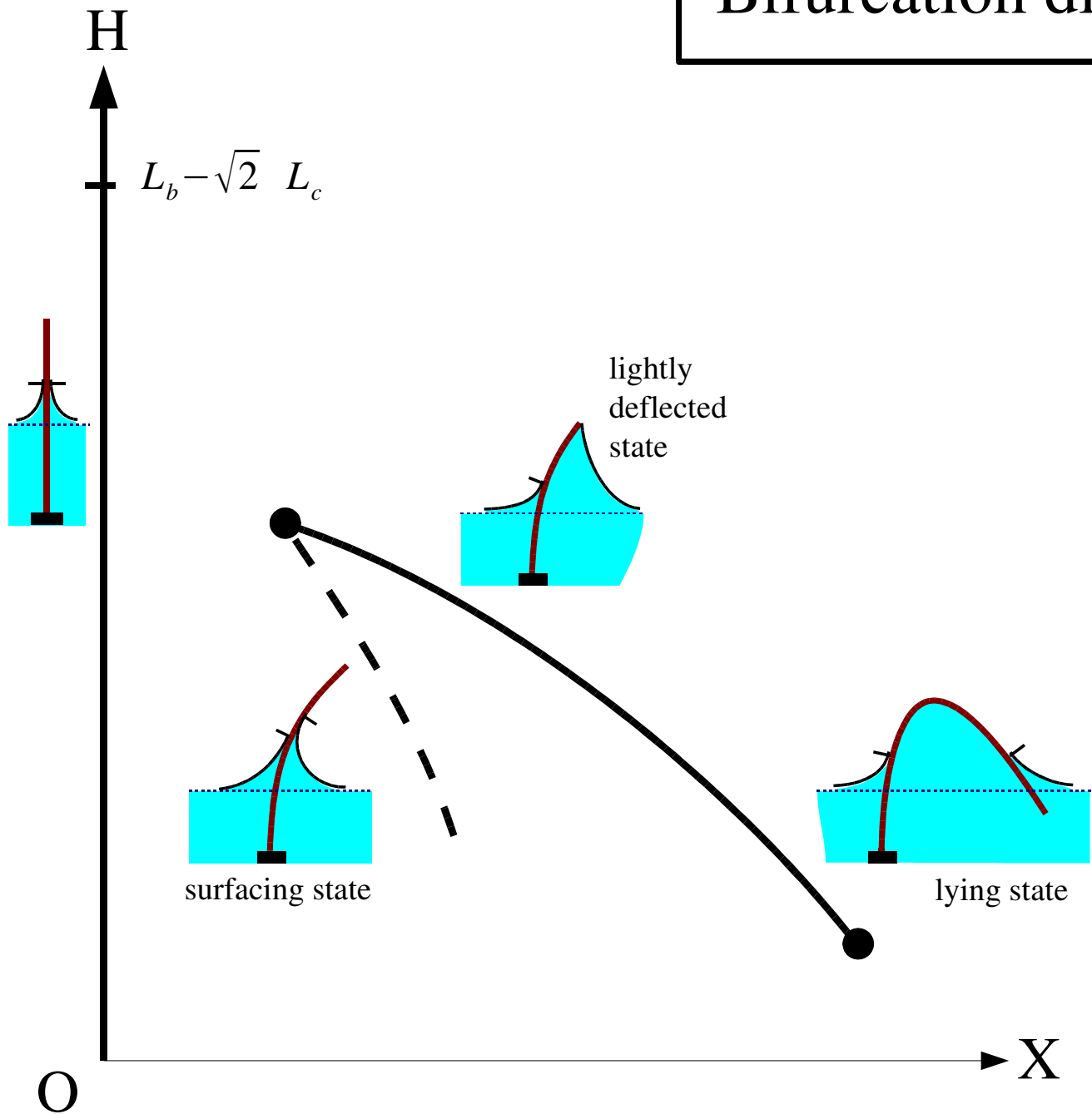
# Bifurcation diagram for $L > L_b$



**hysteresis**



# Bifurcation diagram for $L < L_b$



# Phase diagram

polyester:  $w=2\text{cm}$ ,  $e=25\mu\text{m}$ ,  
 $L_b=1.9\text{cm}$ ,  $L_c=1.5\text{mm}$  (silicone oil)

